

In the Specification

Please amend the paragraph that appears on page 4, line 15 through page 5, line 21 as follows:

Figure 1 is a block diagram of a switched beam beamforming system in accordance with the prior art. An antenna array 12 ~~comprising~~ comprises multiple antennas $12_1, 12_2, \dots, 12_N$ that are arranged at a receiving station 10, e.g., at the top of a cellular telephone system cell tower. The outputs of those antennas are fed into an analog $N \times B$ beamforming circuit 14, wherein N is the number of antennas and B is the number of beams generated by the beamforming circuitry from the antenna signals. The analog beamforming circuitry 14 weighs and combines the RF antenna output signals on lines $13_1, 13_2, \dots, 13_N$ in accordance with a scheme dictated by beamforming control circuit 121 to produce the beam signals $15_1, 15_2, \dots, 15_B$, each beam focused on an angular portion of the reception area. Beamforming circuit 121 may be a DSP executing a predetermined algorithm. The number of beams, B , typically is less than or equal to the number of antennas, N , in the antenna array. Each beam signal $15_1, 15_2, \dots, 15_B$ is passed through frequency down converting circuitry $16_1, 16_2, \dots, 16_B$ for converting the beam signals from the RF frequency range to the baseband range. Each of those signals is digitized by an analog to digital (A/D) converter $18_1, 18_2, \dots, 18_B$. The outputs of the A/D converters are then each input to a fading multipath and multi-user channel estimation circuit, $20_1, 20_2, \dots, 20_B$. Each of those circuits generates L output signals for each of M simultaneous transmitters at use in the given geographic

area, where L is the number of paths per transmitter that the circuitry is designed to process simultaneously (e.g., typically around 3 or 4) and M is the number of simultaneous transmitters using the receive station. Those outputs are input to a minimum variance selector 22 for all of the paths and users. The minimum variance selector generates a path estimate and a path estimate error for each path of each user, i.e., $L \times M$ path estimates and $L \times M$ path estimate errors.

Please amend the paragraph that appears on page 6, lines 7 through 14 as follows:

In the analog $N \times B$ beamforming circuitry 14, for each beam, dedicated RF combining circuitry is necessary, i.e., there are $N \times B$ copies of essentially identical circuitry for processing the N antenna signals beams on lines 15₁, 15₂, ..., 15_B.

RF band hardware is much more expensive than DSPs and other baseband circuitry. Also, as shown in Figure 1, each beam requires a dedicated frequency down converting circuit 16 and a dedicated analog-to-digital converter 18.

Please amend the paragraph that appears on page 11, line 19 through page 12, line 19 as follows:

The N vector channel impulse response from the m th user to the antenna array is given by

$$h_m(t, \tau) = \sum_{l=1}^{L_m(t)} \alpha(\phi_{m,l}) \rho_{m,l}(t) e^{j\psi_{m,l}(t)} \delta(t - \tau_{m,l}(t)) \quad (4)$$

where $L_m(t)$ is the known - possibly time varying - number of resolvable paths.

$\delta(t)$ is the Dirac delta function. ~~$\phi_{m,l}(t)$~~ $\phi_{m,l}$ is the known direction of arrival (DOA)

or angle of arrival (AOA) of the m th user's signal via the l th path. The AOA is measured anti-clockwise from positive real axis. ~~$\rho_{m,l}(t)$~~ $\rho_{m,l}(t)$, ~~$\psi_{m,l}(t)$~~ $\psi_{m,l}(t)$ and $T_{k,l}(t)$ are the signal attenuation, phase shift and time delay of the l th multipath component for user m , respectively, $\alpha(\phi)$ is known as the steering vector, and denotes the response of the antenna array to a signal impinging onto the array from an angle ϕ . For a uniform linear array, the steering vector is given by

$$\alpha(\phi) = [g_1(\phi)\alpha_1(\phi), g_2(\phi)\alpha_2(\phi), \dots, g_N(\phi)\alpha_N(\phi)] \quad (5)$$

where $g_n(\phi)$ denotes the directivity (gain) of the n th antenna element impinging on the array from angle ϕ . Here we assume for illustrative purposes that all the elements have unit directivity, i.e., $g_1(\phi) = \dots = g_N(\phi) = 1$. For our uniform linear array, we have

$$\alpha_n(\phi) = e^{j\pi(n-1)\cos(\phi)}, \forall n \in \{1, \dots, N\} \quad (6)$$

Please amend the paragraph that appears on page 14, line 21 through page 15, line 7 as follows:

Independent Rayleigh distributed multiplicative channel coefficients: We assume the channel coefficients $\alpha_{m,l}(t)$ in Eq. (8) between symbol intervals are modeled as

independent zero-mean circular white Gaussian noise processes and remain constant during each symbol period. In particular, for $n, n' = -\infty, \dots, \infty$, $m, m' \in$

$$\{1, \dots, M\} \text{ and } l, l' \in \{1, \dots, L\} \text{,}$$

$$\alpha_{m,l}(nT_b + \Delta) \sim N(0, \sigma_{m,l}^2)$$

$$\sigma_{m,l}^2) \quad (12)$$

$$\alpha_{m,l}(nT_b + \Delta) = \alpha_{m,l}(nT_b + T_c + \Delta) = \dots = \alpha_{m,l}(nT_b + (G-1)T_c + \Delta) \quad (13)$$

$$V_{k,m,l} = \begin{cases} \chi_{k,m,l}, & \forall k \in \{\dots, -2(G-1), -G-1, 0, G-1, 2(G-1), \dots\} \\ 0, & \text{otherwise} \end{cases}$$

$$E\{\alpha_{m,l}(nT_b + \Delta) \alpha_{m',l'}(n'T_b + \Delta)\} = \delta_{n,n'} \delta_{m,m'} \delta_{l,l'} \delta_{m,l}^2 \quad (14)$$

where $\delta_{k,k'}$ denotes the Kronecker delta function, that is $\delta_{k,k'} = 1$, if $k = k'$, and

$\delta_{k,k'} = 0$ otherwise.

Please amend the paragraph on page 15, lines 15 through 20 as follows:

Discrete-time state-space model: For notational convenience, we rewrite the k th sampled array output after beamforming, given by Eq. (10), as follows

$$Y_k = f_k^H \tau_k + f_k^H W_k \quad (16)$$

where $y_k \triangleq Y(kT_c + \Delta)$, $f_k \triangleq f(kT_c + \Delta)$ and $w_k \triangleq W(kT_c + \Delta)$. Here we use the subscript k to denote the k th sample.

Please amend the paragraph beginning on page 15, line 21 through page 18, line 4 as follows:

Let $\chi_{k,m,l}$ denote the attenuated received spectrum signal at time k

for the m th user via the l th path, i.e.

$$X_{k,m,l} \triangleq b_{k,m}^c c_{k,m} \alpha_{k,m,l} \quad (17)$$

where $\alpha_{k,m,l} \triangleq \alpha_{m,k}(kT_c + \Delta)$. Let

$$V_{k,m,l} = \begin{cases} \chi_{k,m,l}, & \forall k \in \{\dots, -2(G-1), -(G-1), 0, G-1, 2(G-1), \dots\} \\ 0, & \text{otherwise} \end{cases} \quad (18)$$

denote the realization of the attenuated and phase shifted spread spectrum $\chi_{k,m,l}$ every G samples. Since the product $b_{k,m}^c c_{k,m}$ yields ± 1 , and from our statistical assumptions on the channel fading, $V_{k,m,l}$ is complex white Gaussian distributed random variable, such that

$$V_{k,m,l} \sim N(0, \sigma_{m,l}^2), \text{ for } k \in \{\dots, -2(G-1), -(G-1), 0, G-1, 2(G-1), \dots\} \quad (19)$$

and $\forall k, m, l \notin \{\dots, -2(G-1), -(G-1), 0, G-1, 2(G-1), \dots\}$, $V_{k,m,l} = 0$, otherwise. Let

$$h_k = \begin{cases} 0, & \forall k \in \{\dots, -2(G-1), -(G-1), 0, G-1, 2(G-1), \dots\} \\ 1, & \text{otherwise} \end{cases} \quad (20)$$

The attenuated phase shifted received spread spectrum signal $\chi_{k,m,l}$ can be written in the following scalar recursive form

$$\chi_{k,m,l} = h_k c_{k,m} c_{k-1,m,l} \chi_{k-1,m,l} + V_{k,m,l} \quad (21)$$

We group the received signals $\chi_{k,m,l}$ at time index k in a $M \times 1$ vector χ_k as follows

$$\begin{aligned} \chi_k^H &\triangleq (\chi_{k,1,1}, \dots, \chi_{k,1,L}, \dots, \chi_{k,M,1}, \dots, \chi_{k,M,L}) \\ \chi_k^H &\triangleq (\chi_{k,1,1}, \dots, \chi_{k,1,L}, \dots, \chi_{k,M,1}, \dots, \chi_{k,M,L})^H \end{aligned} \quad (22)$$

If we define $V_k^H \triangleq (V_{k,1,1\tau} \dots, V_{k,1,L\tau} \dots, V_{k,M,1\tau} \dots, V_{k,M,L})^H$, then we have

the following vector state equation for the time evolution of the received spread spectrum signals for all user and all paths

$$\chi_k^H \triangleq A_k \chi_{k-1} + V_k \quad (23)$$

where

$$V_k \sim N(0_{ML \times 1}, Q), \forall k \in \{\dots, -2(G-1), -(G-1), 0, G-1, 2(G-1), \dots\} \quad (24)$$

$$V_k = 0, \text{ otherwise} \quad (25)$$

and

$$A_k = \text{diag} \left(\underbrace{h_k c_{k-1,1} c_{k,1}, \dots, h_k c_{k-1,1} c_{k,1}}_{L \text{ Times}}, \dots, \underbrace{h_k c_{k-1,M} c_{k,M}, \dots, h_k c_{k-1,M} c_{k,M}}_{L \text{ Times}} \right) \quad (26)$$

$$Q = \text{diag}(\sigma_{1,1}^2, \dots, \sigma_{1,L}^2, \dots, \sigma_{M,1}^2, \dots, \sigma_{M,L}^2) \quad (27)$$

where A_k and Q are $ML \times ML$ diagonal matrices.

Please amend the paragraph beginning on page 17, line 14 through page 18, line 10 as follows:

Let ϕ denote the vector of all angle of arrivals for all M users.

$$\phi^H = (\phi_{1,1}, \dots, \phi_{1,L}, \dots, \phi_{M,1}, \dots, \phi_{M,L})^H \quad (28)$$

We use $A(\phi)$ to denote the $N \times ML$ matrix response of the array, defined as follows

$$A(\phi) = (a(\phi_{1,1}), \dots, a(\phi_{1,L}), \dots, a(\phi_{M,1}), \dots, a(\phi_{M,L}))^H \quad (29)$$

The ~~$(m-1) \times L=1$~~ $(m-1) \times L=1$ th column vector in $A(\phi)$ corresponds to the

antenna array vector response of a signal impinging onto the antenna array from angle

$\phi_{m,1}$.

Please amend the paragraph appearing on page 18, lines 5 through 10 as follows:

Using Eqs. (23) and (29), the observation Eq. (16) is equivalently written as

$$y_k = f_k^H A(\phi) \chi_k + f_k^H W_k \quad (30)$$

Equations (23) and (30) ~~from~~ form the discrete-time, state-space version of the DS-CDMA beamforming linear antenna array system.

Please amend the paragraph that appears on page 18, line 11 through page 19, line 6 as follows:

1. Optimal Chip-Rate Switched-Beam Design

In this subsection, we formulate the estimation objectives. The aim is to design the time varying switched-beam beamforming vector f_k , such that the minimum estimation error in estimating the received spread spectrum signal χ_k defined in Eq. (22) is obtained. We ~~chese~~ choose the beamforming vector f_k to be a function of the data from time index 0 up to time index k-1, Furthermore, f_k belongs to a set of fixed beam array patterns F . Thus,

$$f_k = f_k(Y_0, Y_1, \dots, Y_{k-1}) \in F \quad (31)$$

for $k = 1, 2, \dots$. The aim is to select the class of beam patterns F and optimally select the sequence of beam-patterns from the set F , such that the estimation errors in estimating the spread spectrum signals are minimized. We chose the following optimization function

$$h_k = E \{ (\chi_k - \chi_{k/k})^H J (\chi_k - \chi_{k/k}) \} \quad (32)$$

where $\chi_{k/k} \triangleq E \{ \chi_k / Y_k \}$ is the conditional mean estimate of χ_k , conditioned on the data $\underline{Y}_k \triangleq (Y_0, Y_1, \dots, Y_k)$, $\underline{Y}_k \triangleq (Y_0, Y_1, \dots, Y_k)$, and J is some predetermined – user defined - weighting matrix. We choose the sequence of optimal beamforming vector $\underline{\hat{f}}_0, \underline{\hat{f}}_1, \underline{\hat{f}}_2, \dots, \underline{\hat{f}}_k$, as follows

$$(\underline{\hat{f}}_0, \underline{\hat{f}}_1, \dots, \underline{\hat{f}}_k) = \arg \max_{\underline{f}_0, \underline{f}_1, \dots, \underline{f}_k} E \{ (\chi_k - \chi_{k/k})^H J (\chi_k - \chi_{k/k}) \} \quad (33)$$

subject to Eq. (31).

Please amend the paragraph that appears on page 20, lines 10 through 12 as follows:

From the previous discussion, we ~~assumed~~ assume $M \times L$ steering vectors associated with $M \times L$ known angle-of-arrivals $\phi_{m,1}$. The set of conventional beamforming array vectors ~~are~~ is given by

$$F_2 = \{ \alpha(\phi_{1,1}), \dots, \alpha(\phi_{1,L}), \dots, \alpha(\phi_{M,1}), \dots, \alpha(\phi_{M,L}) \} \quad (35)$$

Please amend the paragraph that appears beginning on page 20, line 14 through page 21, line 8 as follows:

Optimal Beamforming: The optimal beamforming vector is derived by minimizing the average output power of the beamforming array, while ensuring the unity response in the desired direction s_0 . Assuming $f = f_k$ for all k , we solve the following optimization problem

$$\min_f E\{yy^H\}, \text{subject to } f^H s_0 = 1 \quad (36)$$

Using Lagrange's multiplier method, the optimal beamformer f can be expressed as follows

$$f = \frac{D^{-1}s_0}{s_0^H D^{-1}s_0} \quad (37)$$

where D denotes the average signal, multi-user interference (MUI) plus noise ~~power~~ covariance.

From our statistical assumptions on our signal model, we can show the following result

$$D = A(\phi)QA^H(\phi) + R \quad (38)$$

Note that D is a positive definite matrix since Q and R are positive definite matrices. Thus, the set of optimal beamforming steering vectors are give given by

$$F_3 = \left\{ \frac{D^{-1}\alpha(\phi_{1,1})}{\alpha^H(\phi_{1,1})D^{-1}\alpha(\phi_{1,1})}, \dots, \frac{D^{-1}\alpha(\phi_{1,L})}{\alpha^H(\phi_{1,L})D^{-1}\alpha(\phi_{1,L})}, \dots, \frac{D^{-1}\alpha(\phi_{M,1})}{\alpha^H(\phi_{M,1})D^{-1}\alpha(\phi_{M,1})}, \dots, \frac{D^{-1}\alpha(\phi_{M,L})}{\alpha^H(\phi_{M,L})D^{-1}\alpha(\phi_{M,L})} \right\}$$